# SAAB JA-37 Viggen

# Performance Assessment

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Temporal Images

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## SAAB JA-37 Viggen Performance Assessment

## 1. Overview

The SAAB JA-37 Viggen is a Swedish single seat multi-role fighter. The aircraft is a delta wing design with a canard. Viggen is Swedish for "Thunderbolt". The aircraft has been built in several versions, as follows;

AJ-37 single seat all weather attack JA-37 single seat air defence SF-37 single seat armed photo reconnaissance SH-37 single seat armed sea surveillance SK-37 dual seat conversion trainer

The first flight of the AJ-37 (attack) version was on the 2nd of February, 1967. For the JA-37 (air defence) version, the prototype first flew in June 1974, followed by the first production prototype on the 15th of December 1975, and the first production JA-37 on the 4th of November 1977.

This document is intended to record all the known, freely available weight and dimensional data about the Viggen, then use this information to produce a performance estimate for the aircraft.

## 2. Dimensions

The following figures represent the best data available for the leading dimensions of the aircraft. Note that most dimensions and weights are provided in metric units, then converted to imperial units.

Wing Span Foreplane Span Main Wing Aspect F	10.60 met 5.45 metr Ratio 2.45	34 feet 9.25 in 17 feet 10.5 in		
- 3	45 metres 30 metres	 3.25 inches 5.75 inches		excluding probe) including probe)
- 3	58 metres 40 metres	 .5 inches .75 inches		excluding probe) including probe)
- 3	0 metres 0 metres	25 inches 5 inches	(fin	folded)

Total Lifting Area	52.20 square metres	561.88 sq.ft	(including foreplanes)
Gross Wing Area	46.00 square metres	495.16 sq.ft	(wing alone)
Foreplane Area	6.20 square metres	66.74 sq.ft	(nett)

Note: the gross wing area is the area of the main wing, including that portion which carries across the fuselage. The foreplane area is the area of the lifting surfaces, not including the portion which carries through the fuselage. The "total wing area" defined in some areas is the sum of the gross wing area and nett foreplane area, and can be misleading.

## 3. Weights

Only limited weight data (in metric units) has been provided for the aircraft. The following is my best estimate for the actual weights of the aircraft and its component parts.

Empty Weight	12,200 kg	26,895 lbs	(approx)
Normal Loaded	16,800 kg	37,040 lbs	(carrying four AAM)

Max Takeoff 22,500 kg 49,600 lbs

Up to 6,000 kg (13,227 lbs) of ordnance can be carried externally.

```
Takeoff weight 15,000 kg 33,070 lbs (clean)
Takeoff weight 17,000 kg 37,478 lbs (normal armament)
```

The cannon has 150 rounds, at 0.36 kg (0.79 lbs) per round for a total weight of 54 kg.

```
Weight of Rb-71 (Skyflash) Missile 193 kg 425 lbs Weight of Rb-24 (AIM-9L) Missile 85.3 kg 188 lbs Avionics weight 600 kg 1323 lbs Pilot weight is assumed to be 100 kg
```

Internal fuel 5700 litres 1506 US gal 4440 kg 9789 lbs
External tank 1275 litres 337 US gal 993 kg 2190 lbs (estimated)

(tank weight without fuel = 100 kg - estimated)

Engine Weight 2100 kg 4630 lbs RM-8A 2250 kg 4960 lbs RM-8B

## Weight Breakdown

Assuming the figure of 12,200 kg for a clean, empty aircraft is approximately correct, we can now check one of the other weights to see if it corresponds. An empty aircraft is the condition of the aircraft being fully equipped but with no fuel, pilot or external stores. We have a value for a normal loaded aircraft, which gives us a weight of 17,000 kg when fitted with 4 air-to-air missiles. If we add weights for a pilot and full internal fuel, plus four Rb-24 missiles (AIM-9L), we get the following;

Clean A/C Pilot	12,200 kg 100 kg	(includes 150 rounds for gun)
Fuel (100% internal) 4 x Aim-9L	4440 kg 342 kg	(at 6.5 lbs/US gallon)
_		
Total	17,082 kg	

This corresponds approximately to the weight expected. So we can now propose a weight breakdown for the aircraft and its component parts.

Clean A/C	12,200 kg	(54 kg for 150 rounds for gun)
		(600 kg for avionics)
		(2250 kg for engine)
Pilot	100 kg	
Fuel (100% internal)	4440 kg	(at 6.5 lbs/US gallon)
Rb-24 (AIM-9L)	85.3 kg	
Rb-71 (Skyflash)	193 kg	
External Tank	100 kg	(empty)
External Tank	993 kg	(full)

## 4. Ordnance

The aircraft is typically configured to have up to seven (7) external pylons. These are located as follows (with estimated load limits at each location);

1	х	centreline pylon	2000	kg	4410	lbs
2	х	fuselage edge pylons	500	kg	1102	lbs
2	х	inner wing pylons	1000	kg	2205	lbs
2	Х	outer wing pylons	500	kg	1102	lbs

A typical air defence loading would include 2 x Rb 72 Skyflash and 2 or 4 x Rb 24 Sidewinder (AIM-9L) missiles. The aircraft is fitted with a single 30 mm Oerlikon KCA cannon. This has 150 rounds available.

## 5. Engine

The aircraft is fitted with a Volvo Flygmotor RM-8 turbofan engine. This is based on the Pratt & Whitney JT-8D-22 engine, with a Volvo designed afterburner fitted. The engine has two versions. The RM-8A is fitted to all except the JA version of the aircraft. The JA is fitted with the RM-8B engine; a slightly more powerful version of the engine.

#### Thrust

RM-8A	25,970 lbst	11790 kg	max reheat
	14,750 lbst	6690 kg	max dry
RM-8B	28,110 lbst	12750 kg	max reheat
	16,200 lbst	7350 kg	max dry
Fuel Consumption			
RM-8A	2.47 lb/hr/lbst	70.0 mg/Ns	max reheat
	0.63 lb/hr/lbst	17.8 mg/Ns	max dry
	0.61 lb/hr/lbst	17.3 mg/Ns	max continuous
RM-8B	2.52 lb/hr/lbst	71.4 mg/Ns	max reheat
	0.64 lb/hr/lbst	18.1 mg/Ns	max dry
	0.61 lb/hr/lbst	17.3 mg/Ns	max continuous

#### Dimensions

Length	6.17 metres 6.24 metres	RM-8A RM-8B
Max Diameter Inlet Diameter	1.397 metres 1.030 metres	55 inches 40.55 inches
Max Mass Flowrate	145 kg/sec	

Bypass Ratio 1.10 Max Pressure Ratio 16.5

#### Pratt & Whitney JT-8D-7 Turbofan

For comparison purposes the key performance data for the JT-8 engine are provided here. This is a non-afterburning engine.

6350 kg nett thrust - takeoff - sea level static 1540 kg nett thrust - cruise - Mach 0.80 at 11,000 metres

Cruise sfc 0.81 kg/kg/hour

Bypass Ratio 1.10

Air Flow 141 kg/sec at sea level static conditions

Pressure Ratio 15.8

Internal Diameter 0.108 metres
Length 3.75 metres
Dry Weight 1431 kg

No of Spools 2

## 6. Performance

The following performance and mission profile data is the best estimate from the various sources of data found.

Max Speed at Seal Level (4 x AAM)	838 mph	1350 kmh	Mach 1.10	
Max Speed at 11,000 metres	1365 mph	2195 kmh	Mach 2.1	(at 36,090 ft)
Approach Speed	119 knots	137 mph	220 kmh	

Service Ceiling 60,000 feet

Initial Climb 40,000 fpm (approx)

Time to 32,810 feet (10,000 m)

1.4 minutes (at max afterburner)

#### Mission Profiles

Ferry range 2000 km (2250 km with Jet-A fuel)

Tactical Radius

- intercept mission 250 miles 400 km
- hi-lo-hi profile 621 miles (with unspecified external stores)
- lo-lo-lo profile 311 miles (with unspecified external stores)

For external load of 4 x 1000 lbs (454 kg) bombs and fuel

Tactical Radius

- hi-lo-hi profile 782 miles
- lo-lo-lo profile 532 miles

## 7. Take-Off

The aircraft was initially designed to operate from narrow 500 m long runways (1640 feet). The actual take-off run is approximately 400 metres (1310 feet). The key points in the aircraft take-off are as follows;

Afterburner is selected then the wheel brakes are released.

The aircraft accelerates to a rotation speed of 135 knots (250 kmh).

About 600 metres of runway is used to get airborne.

After lift-off the undercarriage is retracted and the aircraft accelerates at a 2 to 3 degree climb angle to 367 knots (680 kmh).

Below 190 knots (350 kmh) the aircraft is very sensitive in roll.

Afterburner is cut out at 270 knots (500 kmh) due primarily to noise abatement requirements.

Exceeding 30 degrees angle of attack results in some loss of yaw stability.

Over 30 degrees AOA the aircraft will enter into a "super stall", but is easily recoverable.

There is little natural pre-stall warning, with low buffet levels.

## 8. Landing

Landing Run approx 500 m Landing Speed 220 kmh

The undercarriage is lowered.

The thrust reverser is pre-selected to activate immediately after landing.

The approach is steep.

The aircraft attitude is 15 degrees nose up.

The speed is controlled by the autopilot.

The aircraft crosses the runway threshold at 130 knots (240 kmh).

Touchdown with a no-flare landing at 97 knots (180 kmh).

Touchdown is about 45 metres (150 feet) beyond the runway threshold.

The undercarriage is designed for a landing sink rate of 16 feet/sec (5 m/s).

## 9. References

Jane's All the World's Aircraft 1985-86

Modern Combat Aircraft Design by Klaus Huenecke Airlife Publishing Ltd 1987

The Illustrated Encyclopedia of the World's Modern Military Aircraft by Bill Gunston

Salamander Books Ltd 1977

The New Observer's Book of Aircraft by William Green Frederick Warne & Co 1986

Modern Air Combat

by Bill Gunston and Mike Spick

Salamander Books Ltd 1983

Attack Aircraft
by Roy Braybrook
Haynes Publishing Group 1990

World Aircraft Information File - Issue 47 Aerospace Publishing Ltd 1998

Air International - Volume 56 No 2

Key Publishing Ltd February 1999

Aeronautical Vest Pocket Handbook Pratt & Whitney June 1978

## 10. Conversion Factors

The following conversion factors between metric and Imperial units were used at various places in this document.

```
3.281 feet
                            1.0 metre
10.76 square feet
                            1.0 square metres
2.205 pounds
                            1.0 kilogram
                            1.0 US gallon
3.785 litres
4.545 litres
                            1.0 Imperial Gallon
1 knot
                            6080 feet per second
1 mile per hour
                            5280 feet per second
1.097 feet per second =
                            1.0 kilometre per hour
```

## 11. Liquid Weights

The following liquid densities were used to determine the fuel weights for the aircraft.

```
JP-1 6.65 lbs/US gal
JP-3 6.45 lbs/US gal
JP-4 6.55 lbs/US gal
JP-5 6.82 lbs/US gal
Jet-A 6.74 lbs/US gal
Gasoline 5.87 lbs/US gal
Water 8.345 lbs/US gal
```

## Appendix A: Calculated Aircraft Dimensions

The following dimensions and areas have been determined by scanning a 3-view drawing of the Viggen, then importing it into a CAD program, scaling it appropriately and measuring the specific values shown here. Many of these values will be required for a theoretical drag estimation of the aircraft and other aspects of the performance assessment.

No specific wing section data has been found so the values shown are estimates only, based on standard design assumptions.

## Wing

Approximately 4% thick, with maximum thickness at 40% of chord.

Root Chord 24.9 feet Tip Chord 1.8 feet Taper Ratio 0.07

Sweep of Quarter Chord Line 42 degrees
Wing Semi-Span 17.5 feet
Wing Span 35.0 feet
Gross Wing Area 522 square feet

## Foreplane

Approximately 6% thick, with maximum thickness at 40% of chord.

Root Chord 1.0 feet Tip Chord 2.2 feet Taper Ratio 0.20

Sweep of Quarter Chord Line 50 degrees Panel Span 5.3 feet

Panel Area 35.0 square feet

Geometric Aspect Ratio 0.80

#### Vertical Fin

Approximately 5% thick, with maximum thickness at 40% of chord.

Root Chord 13.6 feet Tip Chord 1.6 feet Taper Ratio 0.12

Sweep of Quarter Chord Line 43 degrees Span 9.0 feet

Area 68.7 square feet

Geometric Aspect Ratio 1.20

## Fuselage

Length 50.0 feet Width 8.25 feet Height 7.0 feet

Frontal Area 42 square feet Surface Area 880 square feet

## Appendix B: Calculated Aerodynamic Data

## Calculation of Maximum Lift Coefficient

It is possible to make an estimate of the maximum lift coefficient for the aircraft. Available data states the aircraft approach speed is 119 knots, which will be a speed just above the stall speed of the aircraft.

Assuming 119 knots is the aircraft stall speed, we know the wing area and air density, and can approximate the aircraft weight, and so find the lift coefficient for this condition.

We will assume the atmospheric conditions are for sea level and standard ISA conditions. This gives an air mass density of 0.002378 slugs per cubic foot. Also, 119 knots is equal to 201 feet per second.

We have a gross wing area of 562 square feet. Because the aircraft is of canard configuration, the foreplanes generate lift as well as the main wing, so both contribute to the total aircraft lift.

We will assume a standard weight condition for the aircraft for all subsequent analysis. Much of the tactical radius data obtained is for an aircraft in an air defence configuration, carrying 4 air to air missiles. We will assume this is for two short range ((AIM-9L) and two long range (SkyFlash) missiles. It is also normal practice to assume a 50% fuel load for performance analysis such as this, so we will assume a 50% internal fuel load and no external fuel.

This then gives a weight of 33,244 pounds (15,077 kilograms).

Clean A/C	12,200 kg	J
Pilot	100 kg	J
Fuel (50% internal)	2220 kg	Ð.
2 x SkyFlash	386 kg	Ð.
$2 \times Aim-9L$	171 kg	3
Total	15,077 kg	33,244 pounds

```
CL = (2 \times Weight) / (rho \times area \times velocity \times velocity)

CL = (2 \times 33,244) / (0.002378 \times 562 \times 201 \times 201)

CL = 1.23
```

In practice the actual lift coefficient will be probably be somewhere between 1.25 and 1.30 but a value of 1.23 (based on a reference wing area of 562 square feet) is a safe value for controlled flight at a minimum speed.

## Appendix C: Performance Analysis

Based on the data presented here, a performance estimate for the Viggen has been prepared. This was generated using the suite of computer programs produced by Mr Sidney A Powers, called "BASIC Aircraft Performance" (Kern International, Inc. Copyright 1984).

This suit of programs includes routines to predict aircraft drag, format engine data and determine various aircraft performance parameters, including mission analysis and flight performance at varying altitudes.

#### DRAG ESTIMATE

These routines were used to iteratively obtain a likely drag for the Viggen aircraft, then to determine other data, including flight envelopes at various load factors, turning performance and mission performance for varying stores configurations.

In obtaining a drag estimate for the aircraft it is always necessary to define this in relation to the aircraft's engine performance. The engine performance (thrust and fuel flow, and their variation with speed and altitude) was estimated based on the best data available, but cannot be guaranteed to truly represent the Viggen engine. So the drag data presented is that which corresponds to the engine data used here. If another engine computer model is used to generate engine performance then the drag values may need to be adjusted to suit.

Drag is presented in the typical way for computer analysis, as a profile drag coefficient and a wing spanwise efficiency factor. Together these will define the drag polar for the aircraft. These values have been provided at a range of aircraft speeds, to allow for the relative effects of subsonic, transonic and supersonic flow. That is,

CDo = Profile Drag Coefficient
CDi = Induced Drag Coefficient
CD = Total Drag Coefficient
e = Spanwise Efficiency Factor

CL = Lift Coefficient

AR = Wing Aspect Ratio

Pi = 3.14159

CD = CDo + CDi

where  $CDi = (CL \times CL) / (Pi \times AR \times e)$ 

Initially a set of drag coefficients was obtained using one of the routines provided in the "BASIC Aircraft Performance" suite. Prior use of this program had indicated it provided only a very approximately correct value, and then only at lower speeds. Using this as a starting point these drag data were revised using an iterative procedure. The drag values would be used to generate a flight envelope, then this envelope would be compared with the quoted aircraft performance (stall speed, maximum speed at low level, maximum speed at altitude and service ceiling). The drag data would then be adjusted as required to better match the known performance of the aircraft.

Table 1 shows the geometric data input into the analysis program, and used to obtain the initial drag estimate for the aircraft. Table 2 shows the final drag data obtained after interation, and used for the final performance assessments. Table 3 shows the typical output for one velocity for the "BASIC Aircraft Performance" drag prediction routine, while Table 4 shows the engine data which was used for this analysis.

Figure 1 shows the estimated variation of the aircraft profile drag coefficient with speed, while Figure 2 shows the corresponding wing spanwise efficiency factor and its variation with speed.

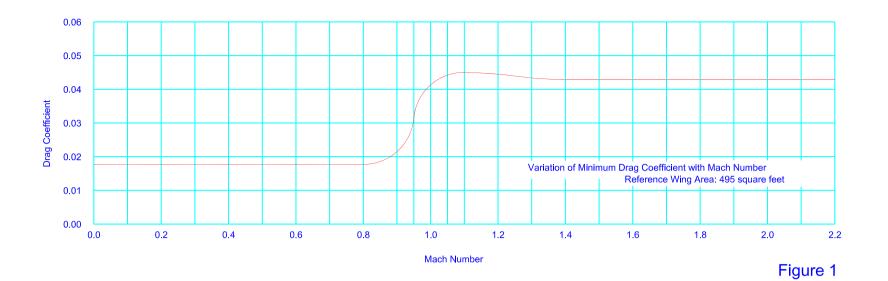
Table 1	FILE: CF)VIGGN
	IDENTIFIER: SAAB JA-37 VIGGEN
	BASIC DATA=============
	ZERO FUEL WEIGHT = 27120
	FUEL WEIGHT = 9790
	NUMBER OF ENGINES = 1
	THRUST MULTIPLIER = 1
	FUEL FLOW MULTIPLIER = 1
	CL(MAX) = 1.25
	WING======
	THEORETICAL AREA = 495.16
	ASPECT RATIO = 2.45
	TAPER RATIO = 0.07
	SWEEP 0F X/C = 42.0
	X/C = 0.25
	(T/C)MAX = 0.04
	X/C LOC OF (T/C)MAX = 0.4
	AIRFOIL RN/C = 1.76304E-03
	HORIZONTAL TAIL===FLAPPED===================================
	EXPOSED AREA = 70.0
	EXPOSED ASPECT RATIO = 0.8
	EXPOSED TAPER RATIO = 0.2
	SWEEP OF X/C = 50.0
	X/C = 0.25
	(T/C)MAX = 0.0b
	X/C LOC OF (T/C)MAX = 0.4
	HEDETCAL TATI STACLE (EL ADDED
	VERTICAL TAIL===SINGLE/FLAPPED===================================
	SINGLE FIN AREA = 68.7
	GEOMETRIC ASPECT RATIO = 1.20
	EXPOSED TAPER RATIO = 0.12
	ZWEEP 0F X/C = 43.0

```
X/C =
                      0.25
           (T/C)MAX =
                      0.05
    X/C LOC OF (T/C)MAX =
                      0.4
WETTED AREA =
             LENGTH =
                      50.0
             WIDTH =
                      8.25
             HEIGHT =
                      7.0
DELTA CDO =
                     0.02
           DELTA F =
                     0.0
         MISC FACTOR =
                     0.25
```

```
Table 2
                                    FILE : DG)VIGGN
                              IDENTIFIER : SAAB JA-37 VIGGEN
                    ****** REVIEW DRAG TABLE ******
                              MACH NO.
                                             CDD
                               0.400
                                           0.01770
                               0.600
                                           0.01770
                               0.800
                                           0.01770
                               0.900
                                           0.02150
                               0.950
                                           0.03140
                               1.000
                                           0.04130
                               1.050
                                           0.04420
                               1.100
                                           0.04500
                               1.200
                                           0.04450
                               1.400
                                           0.04290
                               1.600
                                           0.04290
                               1.800
                                           0.04290
                               2.000
                                           0.04290
                                           0.04290
                               5.500
```

*****	REVIEW WING	E TABLE	*****
	MACII NA	WING E	
	MACH NO-		
	0.400	0.764	
	0.600	0.764	
	0.800	0.764	
	0.900	0.764	
	0.950	0.757	
	1.000	0.695	
	1.050	0.642	
	1.100	0.597	
	1.200	0.526	
	1.400	0.450	
	1.600	0.400	
	1.800	0.361	
	2.000	0.329	
	2.200	0.301	

```
Table 3
                                                   FILE: DG)TEST
                                                   SAAB JA-37 VIGGEN
                                               SUBSONIC ZERO-LIFT DRAG
                                                     M = 0.600
                                                     ALT = 0
                                                   RN/FT = 4.26E+06
                                             REFERENCE WING AREA = 495.2
                                                            FORM
                                                                          INTERF
                       COMPONENT
                                   SWET
                                          LENGTH
                                                     RN
                                                           FACTOR
                                                                           FACTOR
                       WING
                                    609.2
                                           13.91 5.93E+07 1.048
                                                                 0.00217
                                                                           1.143 0.00000 0.00319 1.580
                       HORIZONTAL
                                    143.2
                                           10.74
                                                  4.58E+07
                                                           1.073
                                                                  0.00225
                                                                           1.351
                                                                                  0.00000
                                                                                          0.00094
                       VERTICAL
                                    140.0
                                            9.12 3.89E+07
                                                                  0.00537
                                                                           1.340 0.00000
                                                           1.060
                                                                                          0.00093
                                                                                                   0.459
                       FUSELAGE
                                    880.0
                                           50.00 2.13E+08 1.227
                                                                  0.00181
                                                                           1.015 0.00000
                                                                                          0.00400
                                                                                                   1.980
                       · JZIM
                                     0.0
                                            0.00 0.00E+00 0.000 0.00000
                                                                           0.000 0.00000
                                                                                          0.00866
                                                                                                  4.290
                       TOTAL
                                  1,772.3
                                                                                          0.01772 8.776
                                                     CFE = 0.00495
                                             SPAN EFFICIENCY FACTOR = 0.915
```



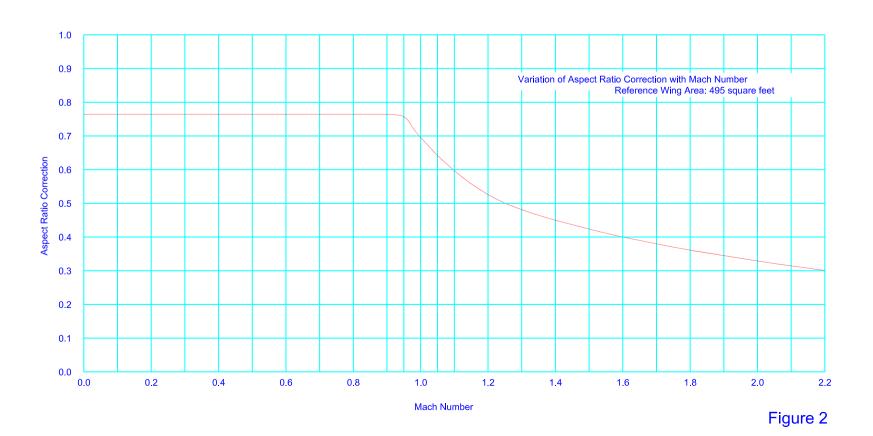


Table 4	FILE :F IDENTIFIER NO OF ALTITUD	:VOLVO FLYGMOTOR	RM-8B	TURBOFAN
MACH	: EQUTITLA TEURHT	O FEET FUEL FLOW		
0.000	22,650 14,164 8,758	57,078 9,065 5,342		
0.400	24,414 12,657 7,474	61,523 8,100 4,559		
0.800	28,836 11,311 6,174	72,666 7,239 3,766		
0.900	30,827 10,988 5,676	77,684 7,032 3,462		
1.000	32,421 10,090 4,125	81,700 6,458 2,516		
1.100	45,740 8,456 1,435	115,265 5,412 875		
7.200	37,268 6,398 0	93,915 4,095 0		
MACH	OL: 3 UTITLA TZURHT	¬OOO FEET FUEL FLOW		
0.400	19,435 8,725 5,154	48,976 5,584 3,144		
0.600	21,123 8,864 5,140	53,230 5,673 3,135		

0.800	23,740 9,120 5,120	59,825 5,837 3,123
0.900	25,187 9,224 4,989	63,471 5,903 3,043
1.000	26,582 9,080 4,281	66,987 5,811 2,611
7.500	28,190 7,243 458	71,039 4,636 279
7-600	39,792 0	100,276 0
MACH	ALTITUDE : 2	0,000 FEET FUEL FLOW
0.400	14,106 5,913 3,420	35,547 3,784 2,086
0.600	15,616 6,017 3,484	39,352 3,851 2,125
0.800	18,050 6,503 3,715	45,486 4,162 2,266
0.900	19,367 6,861 3,773	48,805 4,391 2,302
1.000	20,608 6,966 3,479	51,932 4,458 2,122
1.200	23,932 6,331 1,726	60,308 4,052 1,053

1.800	41,742 0	%105 <sub>7</sub> 190 0	
MACH	E : B⊄UTITJA TZURHT	BO,OOO FEET FUEL FLOW	
0.400	9,040 3,971 2,283	22,781 2,541 1,393	
0.800	12,550 4,408 2,476	31,626 2,821 1,510	
0.900	13,709 4,651 2,562	34,547 2,977 1,563	
1.000	14,880 4,610 2,301	37,497 2,950 1,404	
1.200	18,162 5,173 1,821	45,768 3,311 1,111	
1.800	30,458 0	76,754 0	
2.200	38,404 0	96,778 0	
MACH	ALTITUDE : 4 TRUST	FUEL FLOW	
0.600	6,404 2,733 1,631	16,138 1,749 995	
0.800	7,521 3,046 1,747	18,953 1,949 1,066	
0.900	8,133 3,151 1,744	20,495 2,017 1,064	

1.000	8,953 3,097 1,578		
7.500	12,054 3,163 1,066		
2.000	24,957 0	62,891 0	
2.400	31,360 0	79,027 0	
MACH 	ALTITUDE : ! THRUST	50,000 FEET FUEL FLOW	
0.700	4 <sub>7</sub> 570 0	11,516 0	
0.900	5,273 0	13,288 O	
1.000	5,865 O	14,780 0	
1.200	6,990 0	17,615 O	
1.600	11,313 O	28 <sub>1</sub> 508 0	
2.000	14,928 0	37,618 O	
5.600	16,968 0	42,759 0	
MACH	ALTITUDE : E	O O O O FEET  FUEL FLOW	
0.800	3,590 0	9,047 0	
1.000	3,890	9,803	

	0	0
1.200	4 - 495 0	11,327 0
1.400	4 - 8 1 8 O	12,141 O
1.600	5 <sub>7</sub> 500 0	13,860 0
5.000	7,468 0	18,819 O
2.200	058 r 8 0	0 22,226

#### PERFORMANCE ESTIMATE

Once a specific set of drag and thrust data has been defined, for a particular aircraft geometric configuration, it is possible to determine the aircraft's performance. The most useful initial performance data is the aircraft flight envelope. For the Viggen. this has been estimated for a number of load factors. Table 5 shows the flight envelope data generated by the performance analysis program, while Figure 3 presents the flight envelope in a graphical form. The flight envelope approximates to the published performance values for the aircraft in terms of maximum speeds, stall speed and expected service ceiling.

Table 5	FLIGHT ENVELOPE
	CONFIGURATION FILE : CF)VIGGN
	AIRCRAFT : TAAN TOTOMOTOR RAAZ : TAAN TOTOMOTOR RAAZ : USE TO TOTOMOTOR RAAZ : TANDOT RAAD OVER THE TOTOMOTOR RAAZ : TANDOT RAAD OVER TANDOT R

LOAD	FACTOR =	l l			
ALTITUDE	<mini M KTA</mini 	Z KEAZ	<m< td=""><td>MUMIXAN KTAS</td><td></td></m<>	MUMIXAN KTAS	
10.000 15.000 25.000 30.000 40.000 45.000 50.000 51.000 53.000	0.187 12 0.205 13 0.225 14 0.249 15 0.275 16	4 124 4 124 6 124 9 124 4 124 2 124 8 127 3 141 4 152 8 165 6 167 3 169	1.123 1.091 1.173 1.485 1.635 1.762 1.919 2.099 1.981 0.987	730 696 735 912 984 %1039 %1106 %1204 %1136 584 572 564 556	678 599 583 667 660 637 618 599 502 229 219 211
LOAD	FACTOR =	2			
ALTITUDE	<mini M KTA</mini 	Z KEAS	M	KTAS	KEAZ
5,000 10,000 15,000 20,000 25,000 30,000	0.264 17 0.290 18 0.318 20 0.351 22 0.397 24 0.484 29 0.584 34 0.726 41	5 175 8 175 3 175 0 175 4 178 1 195 4 211 9 234	1.113 1.068 1.123 1.311 1.504 1.594	724 682 703 805 906 939 578	672 586 558 589 607 576 323

LOAD	FACTOR	= 3						
	<	MINIMUM	>	<	MAXIMUM	>		
ALTITUDE	M	KTAS	KEAS		KTAS	KEAZ		
0 5,000				1.123 1.058				
				1.036				
15,000	0.492	309	245	1.049	657	522		
20,000	0.588 0.700	367	264	1.051 1.006	646	472 406		
25,000 30,000	U•7UU O•845	119A	205 283	1.006 0.952	6U B	406 344		
35,000	0.000	0 .	0	0.000				
4401	FACTOR	= 4						
LVAD	TACTOR	•						
				<>				
ALTITUDE	M 	KTAS	KEAS	M 	KTAS	KEAS		
0	0.413	273	273	0.989	654	654		
5,000								
10,000 15,000								
50,000	D.633	407 47N	363 343	0.990 0.968	660 594	492 434		
25,000	0.000	0	0	0.968 0.000	0			
LOAD	FACTOR	= 5						
ALTITUDE	<			<	MAXIMUM KTAS	>		
ALITIONE		V I W 7						
0	0.517	342	342	0.000	0	0		
5,000	0.598	389	361	0.976	635	589		
10,000 15,000	U.672	442 507	403	0.968 0.939	549 549	531 467		
50,000	0.000	0	0	0.000	0	0		

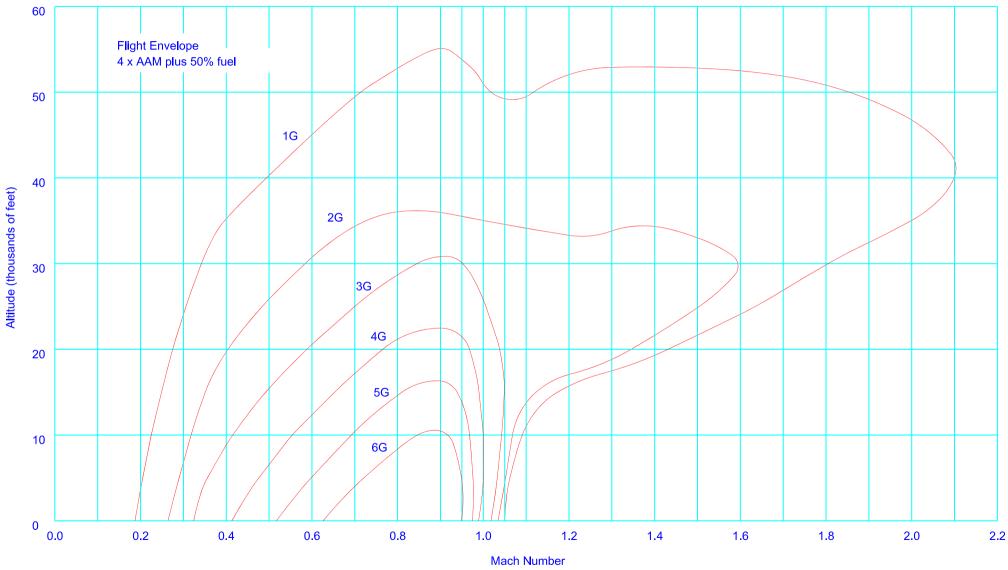


Figure 3

LOAD	FACTOR	= L					
	<	MINIMUM	>	<	MAXIMUM	1>	
ALTITUDE	M	KTAZ	KEAZ	M	KTAS	KEAS	
0	0.656		414	0.000	0	0	
5,000	0.721		435		617		
	0.846		464		586		
15,000	0.000	0	0	0.000		0	
LOAD	FACTOR	= 7					
	<	MINIMUM	>	<>			
ALTITUDE	M	KTAS	KEAS	M 	ZATX	KEAS	
П	0.744	492	492	п.933	617	617	
5,000		584			586		
10,000	0.000		0	0.000		0	
		_	_		_	_	

In an attempt to verify the performance data estimated here with the published performance figures a ferry mission was defined. Table 6 shows the specific legs making up this ferry mission, while Figure 4 displays the results obtained from the analysis program. The published figures indicate a ferry range for the aircraft of 1250 miles (2000 kilometres). The computer prediction gives calculated a ferry range of 1088 miles (945 nautical miles).

Table 6	MISSION DESCRIPTION MI)FERRY
	VIGGEN FERRY MISSION
ZEG	DESCRIPTION
	ALLOW FUEL FOR 1 MIN AT FULL THROTTLE  5 MIN AT IDLE THRUST
2	
_	CLIMB TO 35000 FEET AT MAX R/C ** RANGE BALANCE FOLLWING SEGMENT
4 5	
Ь	ALLOW FUEL FOR 1 MIN AT FULL THROTTLE 5 MIN AT IDLE THRUST

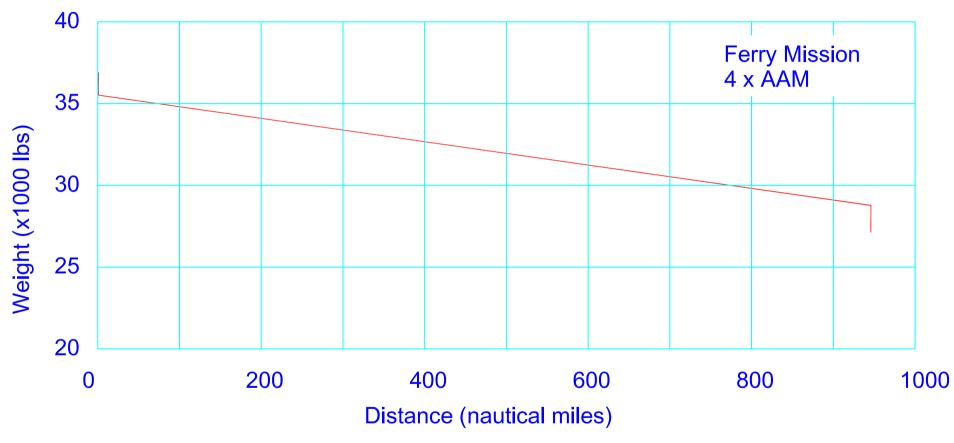


Figure 4

Further checking of the drag data estimated here was carried out by comparing a climb to altitude. This information was provided in the published data for the aircraft, with a climb to 32,810 feet (10,000 metres) quoted as taking 1.4 minutes (84 seconds), for an aircraft loaded with four AAM stores plus 50% internal fuel, and climb performed at maximum afterburner. The analysis program indicated a time to 32,000 feet, for the same aircraft configuration, would take 1.7 minutes (102 seconds). The program output for this climb is presented in Table 7, with Figure 5 showing the actual, and estimated, time to climb in a graphical format.

able 7					CL	IMB VER	IFICATI	٥N							
					FILE		: (F)V	IGGN							
					AIRCR	AFT	: SAAB	JA-37 \	IGGEN						
					ENGIN			O FLYGMO		<b>BB TURB</b>	OFAN				
					IZZIM	0 N	: CLIM	IB TO 328	10 FEET						
					S(REF	)	: 495								
					AR	FNETNE	. 2.4	5							
					NO OF	ENGINE	.Х: Т								
												FUEL			
TIME	ALT	RANGE	WEIGHT	FUEL	ZAT	EAS		R/C	SR			FLOW			
MIN	FΤ	NM	LBZ	LBZ	KTZ	KTZ	MACH	FT/MIN	NM/LB	CL	CDO	LB/HR	TZURHT	Ε	L/D
0.0		п	36,910	9,790	0.0	0.0	0.000	0	0.0000	0.000	0.00000			0.000	0.0
	_	EET AT BE					0.000		0.000	0.000	0.0000	J	5	0.000	5-5
0.0			36,910	9,790	555.4	555.4	0.840	29,327	0.0074	0.071	0.01921	74,654	29,625	0.764	3.6
0.1	2,000	l	36,826	9,706	551.3	535.4	0.839	28,660	0.0076	0.077	0.01919	72,181	28,604	0.764	3.8
0.1	4,000	l	36,742	9,622	551.0	519.3	0.845	27,906	0.0079	0.081	0.01940	69,826	27,654	0.764	4.0
0.2	6,000		36,659	9,539	551.5	504.4	0.851		0.0085	0.086	0.01966		26,691	0.764	4.1
0.3	8,000		36,576	9,456	552.5	490.0		56,195	0.0085	0.091	0.01995		25,711	0.764	4.3
0.4	10,000		36,493	9,373	553.7	476.1		25,231	0.0089	0.096	0.0505P		24,716	0.764	4.4
0.4	75,000		36,411	9,291	555.5	462.8	0.877		0.0093	0.101	0.050P5		53,660	0.764	4.5
0.5	14,000		36,329	9,209	541.5	436.9		55-869	0.0096	0.114	0.02002		55,560	0.764	5.1
0.6	16,000		36,247	9,127	537.1	419.5		57-663	0.0707	0.753	0.05007		21,097	0.764	5.4
0.7	18,000		36,165	9,045	536.8	405.7		20,524	0.070P	0.131	0.02025		20,046	0.764	5.7
0.8	20,000		36,085	8,962	538.1	393.3		19,419	0.0775	0.139	0.02058		19,050	0.764	5.8
0.9	55,000		35,999	8,879	538.6	380.5		18,105	0.0119	0.148	0.02088		17,927	0.764	P • 0
1.0	24,000		35,916	8,796	528.6	360.8		16,615	0.0756	0.165	0.02053		16,633	0.764	b·5
7.5	56,000		35,831	8,711	525.0	345.9		15,295	0.0134	0.179	0.02058		15,524	0.764	6.9
1.3	58,000		35,745	8,625	525.8	334.2		14,120	0.0143	0.191	0.02091		14,556	0.764	7.0
1.4	30,000		35,657	8,537	524.8	321.7		12,945	0.0153	0.205	0.02114		13,599	0.764	7.3
7.5	35,000		35,566	8,446	514.4	303.9		11,104	0.0768	0.530	0.02076		12,185	0.764	7.7
1.7	35'970		35,529	8,409	513.0	298.5	0.887	70,465	0.0175	0.539	0.02079	54,335	11,697	0.764	7.8
1.381	< D	ELTA FUEL													

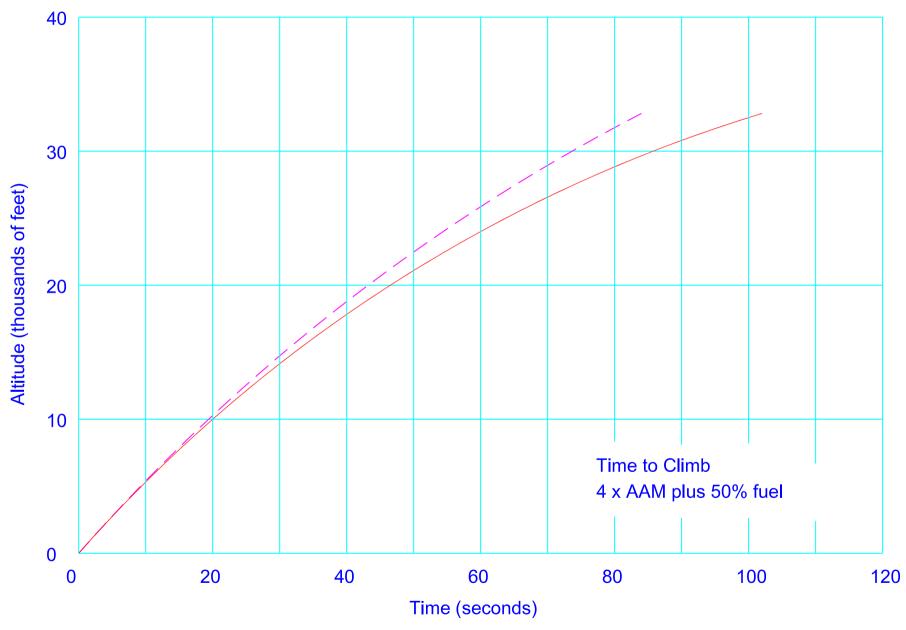


Figure 5

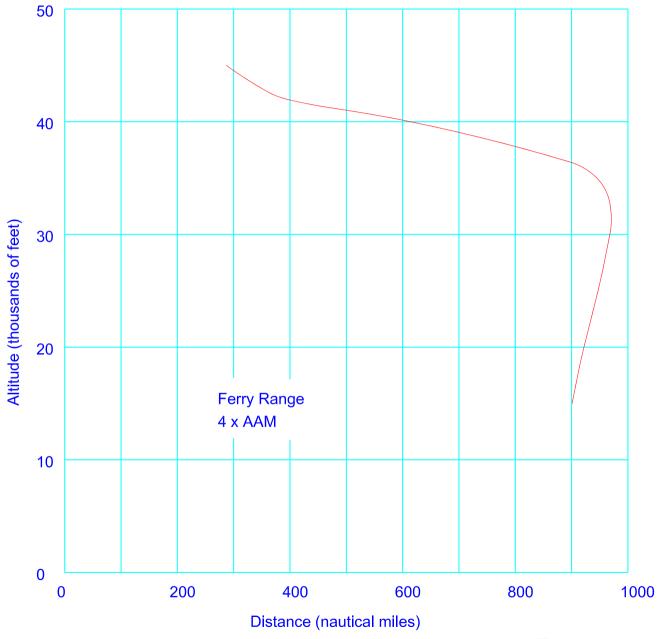


Figure 6

As there was a discrepancy with the actual and calculated ferry ranges (1250 miles compared with 1088 miles), a little further investigation was carried out. The actual ferry range was at an unspecified cruising altitude, so the ferry mission was run for a range of different cuise altitudes. The results of this analysis are shown in Figure 6. This indicated a maximum achievable range of about 960 nautical miles (1105 miles), which is about 13% less than the published figure for tha actual aircraft.

Overall, the discrepancies in the ferry range and climb performance are most likely due to the use of less than perfect engine performance data. Better engine data would probably give a closer match to the actual aircraft performance. At present, the engine and drag data currently used in the computer analysis program will give conservative performance results.

Finally, a table of data has been provided to define the predicted manoeuvre performance of the aircraft. This data is for a range of velocities and altitudes, and is presented in Table 8. Estimates are given for maximum turnrate, specific excess power, specific range and a few other parameters.

able 8	3			MANOEUV	RE PERF	RMANCE			
			CONF	IGURATI	ON FILE	: CF)VIG	GN		
			ENGINE NO OF E S(REF) ASPECT AIRCRAF	T NGINES RATIO T WEIGH'	: VOL : 1 : 495. : 2.45 [: 3201	16	GGEN IOTOR RM-	åB TURB≬	FAN
			LICENT		ITUDE =	0			
	<						CRUIS	E POWER-	
MACH	CL-M	N-MAX					F FLO B LB/HR		
0.20 0.30 0.40 0.50 0.60 0.70 0.80 0.90		2 · 58 3 · 88 4 · 84 5 · 77 6 · 64 7 · 44 7 · 84		0.3 0.8 0.9 0.8 0.8 0.8	571.0	0.0980 0.1402 0.1409 0.1261	3,813 2,025 1,887 2,347 3,148 4,198 5,461 14,438 75,413		1.091* 0.485* 0.273 0.175 0.121 0.089 0.068 0.054

< N = ]									
	<pre>&lt;&gt; TRATE TR/FF P-SUB-S SUBSTANT TRUBLE  **TRATE TR/FF P-SUB-S SUBSTANT TR/FT  **TRATE TR/FT  **TRATE</pre>								
MACH	CL-M	N-MAX	DEG/S		FT/SEC	NM/LB	LB/HR		G CL-C
0.30		1.77	8.4			0.0686			0.704*
0.40	1.145	2.89			573.3	0.1537	2,074	3,587	0.396
0.50	0.917	3.62	11.9	0.8	280.4	0.1524		3,615	0.254
0.60	0.761	4.32	75·5 75·7 75·0	0.8	342.2	0.1545	2,478	4,177	0.176
0.70	0.655	5.06	15.1	0.8		0.1442	3,098 3,896	5,084	0.129
0.80	0.573	5.78	12.2	0.7	47O.6				0.099
0.90	0.485	P·50	11.6		483.6		5,901		0.078
1.00	0.246	3.88	6.4		179.9		48,299		0.063
1.10	0.000	1.00	0.0	0.0	-17.6	0.0099	70,729	27,862	0.052
					JDE = 20L		- N = 1		>
	<			JER	<	> <	CRUIS	E POWER-	>
M A C.I.			T RATE	JER TR∕FF	> ::	 > < S Z Z	ZIURO F FL0	E POWER- W THRUS	> T
M A C H	CL-M		T RATE	JER TR/FF DEG/LG	> ::	> < > RNG Z Z RNG	CRUIS F FL0 LB/HR	E P≬WER- ZURHT W LB/EN	> T G CL-C
0.30	CL-M	N-MAX	T RATE DEG/S	JER TR/FF DEG/LG	< P-SUB-: FT/SEC 	> < > C RNG BN/NN 	CRUIS F FLO LB/HR  5,355	E POWER- W THRUS LB/EN  L,2L9	T G CL-C 1.053*
0.30 0.40	CL-M	N-MAX	T RATE DEG/S	JER TR/FF DEG/LG	< P-SUB-: FT/SEC  &&& 18.4	> < > NR 2 Z BA\MN  44E0-0	CRUIS F FLO LB/HR  5,355 2,604	E POWER- W THRUS LB/EN  6,269 4,181	T G CL-C  1.053* 0.592
0.30 0.40 0.50	CL-M	N-MAX	T RATE DEG/S	JER TR/FF DEG/LG	< P-SUB-: FT/SEC  &&& 18.6 183.0	> < > C S NM B B NM/LB  44E0.0 44P0.0	CRUIS F FLO LB/HR  5,355 2,604 2,178	E POWER- W THRUS LB/EN  6,269 4,181 3,558	> T G CL-C  1.053* 0.592 0.379
0.30 0.40 0.50	CL-M  1.250 1.196 0.964 0.807	N-MAX  1.19 2.02 2.55 3.07	T RATE DEG/S 3.8 7.8 8.3	JER TR/FF DEG/LG  D-4 D-8 D-8	< P-SUB-: FT/SEC  L8.8 128.6 128.6	> < S RNG Z SNG NM/LB  0 12 12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	CRUIS F FLO LB/HR  5,355 2,604 2,178 2,195	E POWER- W THRUS LB/EN  6,269 4,181 3,558 3,586	T G CL-C 1.053* 0.592 0.379 0.263
0.30 0.40 0.50 0.60	CL-M  1.250 1.196 0.964 0.807	N-MAX  1.19 2.02 2.55 3.07 3.63	T RATE DEG/S 3.8 7.8 8.3 8.6	JER TR/FF DEG/LG  0 · 4 0 · 8 0 · 8 0 · 8	< P-SUB-: FT/SEC  &&.& 128.6 128.0 233.8 291.3	> < S	CRUIS F FLO LB/HR  5:355 2:604 2:178 2:195 2:457	E POWER- W THRUS LB/EN 6,269 4,181 3,558 3,586 3,984	T G CL-C 1.053* 0.592 0.379 0.263 0.193
0.30 0.40 0.50 0.60 0.70	CL-M  1.250 1.196 0.964 0.807 0.703	N-MAX  1.19 2.02 2.55 3.07 3.63 4.20	T RATE DEG/S 3.8 7.8 8.3 8.6 4.7	JER TR/FF DEG/LG  0	< P-SUB-: FT/SEC  &&.& 128.6 128.6 183.0 233.8 291.3	> < S RNG NM/LB  0.0344 0.0944 0.1410 0.160 0.1750 0.1700	CRUIS F FLO LB/HR 5:355 2:604 2:178 2:195 2:457 2:891	E POWER- W THRUS LB/EN 6,269 4,181 3,558 3,586 3,984 4,634	T G CL-C 1.053* 0.592 0.379 0.263 0.193 0.148
0.30 0.40 0.50 0.60 0.70 0.80	CL-M  1.250 1.196 0.964 0.807 0.703 0.622 0.538	N-MAX  1.19 2.02 2.55 3.07 3.63 4.20 4.60	T RATE DEG/S 3.8 7.8 8.3 8.6 8.7 8.7	JER TR/FF DEG/LG  0 · 4 0 · 8 0 · 8 0 · 8 0 · 8 0 · 8	< P-SUB-: FT/SEC  68.8 128.6 128.6 233.8 291.3 347.6 374.4	> < > S RNG NM/LB  0.0344 0.0944 0.1410 0.1450 0.1680 0.1750 0.1700 0.1329	CRUIS F FLO LB/HR 5:355 2:604 2:178 2:178 2:195 2:457 2:891	E POWER- W THRUS LB/EN 6,269 4,181 3,558 3,586 3,984 4,634 6,522	T G CL-C 1.053* 0.592 0.379 0.263 0.193 0.148
0.30 0.40 0.50 0.60 0.70 0.80 0.90	CL-M  1.250 1.196 0.964 0.807 0.703 0.622 0.538 0.324	N-MAX 1.19 2.02 2.55 3.07 3.63 4.20 4.60 3.42	T RATE DEG/S 3.8 7.8 8.3 8.6 8.7 9.1	JER TR/FF DEG/LG 0	< P-SUB-: FT/SEC  68.8 128.6 128.6 233.8 291.3 347.6 374.4	> < > S RNG NM/LB  0.0344 0.0944 0.1410 0.1680 0.1750 0.1700 0.1329 0.0200	CRUIS F FLO LB/HR 5:355 2:604 2:178 2:178 2:195 2:457 2:891 4:162 30:761	E POWER- W THRUS LB/EN 6,269 4,181 3,558 3,586 3,984 4,634 6,522	T G CL-C 1.053* 0.592 0.379 0.263 0.193 0.148 0.117
0.30 0.40 0.50 0.60 0.70 0.80	CL-M  1.250 1.196 0.964 0.807 0.703 0.622 0.538	N-MAX  1.19 2.02 2.55 3.07 3.63 4.20 4.60	T RATE DEG/S 3.8 7.8 8.3 8.6 9.1 8.9 9.1	JER TR/FF DEG/LG 0.4 0.8 0.8 0.8 0.8 0.7 0.7	< P-SUB-: FT/SEC  68.8 128.6 128.6 233.8 291.3 347.6 374.4	> < > S RNG NM/LB  0.0344 0.0944 0.1410 0.1450 0.1680 0.1750 0.1700 0.1329	CRUIS F FLO LB/HR 5:355 2:604 2:178 2:178 2:195 2:457 2:891	E POWER- W THRUS LB/EN 6,269 4,181 3,558 3,586 3,984 4,634 6,522	T G CL-C 1.053* 0.592 0.379 0.263 0.193 0.148
0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00	CL-M  1.250 1.196 0.964 0.807 0.703 0.622 0.538 0.324 0.208	N-MAX 2.02 2.55 3.07 3.63 4.20 4.60 3.42 2.66	T RATE DEG/S 3.8 7.8 8.3 8.6 9.1 8.9 5.8 4.0	JER TR/FF DEG/LG 0.4 0.8 0.8 0.8 0.7 0.7 0.7 0.4	< P-SUB-: FT/SEC  68.8 128.6 128.6 233.8 291.3 347.6 374.4 197.0	> < S S RNG NM/LB  0.0344 0.0944 0.1410 0.1680 0.1750 0.1750 0.1329 0.0200 0.0149	CRUIS F FLO LB/HR 5:355 2:604 2:178 2:195 2:457 2:891 4:162 30:761 45:263	E POWER- W THRUS LB/EN 6,269 4,161 3,556 3,566 3,984 4,634 6,522 14,524 18,947	T G CL-C 1.053* 0.592 0.379 0.263 0.193 0.148 0.117 0.095
0.30 0.40 0.50 0.60 0.70 0.80 0.90 1.00	CL-M  1.250 1.196 0.964 0.807 0.703 0.622 0.538 0.324 0.208	N-MAX 2.02 2.55 3.07 3.63 4.20 4.60 3.42 2.66 2.09	T RATE DEG/S 3.8 7.8 8.3 8.6 9.1 8.9 9.1	JER TR/FF DEG/LG 0.4 0.8 0.8 0.8 0.7 0.7 0.7 0.4	< P-SUB-: FT/SEC  L8.6 128.6 128.6 291.3 347.6 374.4 197.0 118.4 68.2	> < S S RNG NM/LB  0.0344 0.0944 0.1410 0.1680 0.1750 0.1700 0.1329 0.0200 0.0149 0.0135 0.0123	CRUIS F FLO LB/HR 5,355 2,604 2,178 2,195 2,457 2,891 4,162 30,761 45,263 54,696 64,947	E POWER- W THRUS LB/EN 6,269 4,181 3,558 3,586 4,634 4,634 6,522 14,524 18,947 22,176	T G CL-C 1.053* 0.592 0.379 0.263 0.193 0.148 0.117 0.095 0.078

				ALTIT	JDE = 3	30000			
MACH	<	N-MAX	T RATE	TR/FF	 -BUZ-9 )32\T7	> < > RNG Z Z NM/LB	CRUIS F FL0 LB/HR	E POWER- ZHRUS LB/EN	> T G CL-C
0.40 0.50 0.60 0.70 0.80 0.90 1.00 1.10 1.20 1.30 1.40 1.50	1.189 0.981 0.838 0.732 0.650 0.573 0.378 0.283 0.231 0.203 0.177 0.146 0.113	1.30 1.68 2.06 2.45 2.84 3.17	3.9	0.6 0.7 0.7 0.6 0.4 0.2 0.2 0.1	42.8 89.5 134.0 177.2 219.4 249.3 154.3 128.7 124.4 133.9 138.0 119.0 86.3	0.0261 0.0945 0.1547 0.1654 0.2001 0.1526 0.0284 0.0222 0.0203 0.0163 0.0170 0.0157	9,040 3,118 2,285 2,225 2,356 3,475	5,599 4,155 3,607 3,523 3,723 4,794 9,912 12,756 14,824 16,897 19,088 21,756 24,624 27,680	
				ALTITU	JDE = 4		– N = 1.		>
MACH	CL-M		DEG/S	DEG/LG	FT/SE(	NM/LB	LB/HR	LB/EN	G CL-C
0.50 0.60 0.70 0.80 0.90 1.00 1.10 1.20		1.01	0.6 2.4 3.0 3.4 2.2 2.0	0.2 0.5 0.6 0.6	2.1 36.1 67.2 96.3 113.7 57.6 56.9	0.0204 0.0413 0.0754 0.1198 0.1033 0.0362 0.0301	14,070 8,333 5,325 3,829 4,998 15,865 20,985 20,985 23,974 27,964	5,705 4,413 3,788 3,541 3,955 7,048 8,792	0.937* 0.651* 0.478 0.366 0.289 0.234 0.194 0.163

```
1.40 0.221
             1.85
                    2.1
                            0.2 113.5
                                        0.0251 32,024 12,599 0.119
1.50 0.198
             1.91
                    2.1
                            0.2 121.5
                                        0.0234
                                               36,723 14,214
                                                              0.104
1.60 0.175
             1.92
                    1.9
                            0.2 122.9
                                        0.0221
                                               41,540 15,965
                                                              0.091
                            0.1 117.4
                                        0.0570
                                               46,394 17,835
1.70 0.153
             1.89
                    1.8
                                                              0.081
                            0.1 103.5
1.80 0.131
             1.81
                                               51,284 19,835 0.072
                    1.6
                                        0.0507
1.90 0.108
             1.67
                    1.3
                            0.1
                                 79.9
                                        0.0194
                                               56,151 21,954
                                                              0.065
                                        0.0188 60,981 24,199 0.059
2.00 0.083
             1.42
                    1.0
                            0.1
                                 45.8
2.10 0.053
             1.00
                    0.0
                            0.0
                                 -0.4
                                        0.0180 66,943 26,565 0.053
                           ALTITUDE = 50000
                                 <----> N = 1 ---->
     <----> <-----> <----> CRUISE POWER----->
                                 P-SUB-S S RNG
                  T RATE TR/FF
                                                 F FLOW
                                                        THRUST
MACH CL-M N-MAX DEG/S
                          DEG/LG FT/SEC
                                          NM/LB
                                                 LB/HR
                                                         LB/ENG CL-C
0.60 0.842
             1.00
                    0.0
                            0.0
                                -36.9
                                        0.0218 15,758
                                                        6,253 1.049*
                                 -7.7
                                        0.0323 12,430
0.70
     0.737
             1.00
                    0.0
                            0.0
                                                        4,933 0.771*
                                        0.0436 10.518
0.80 0.655
             1.11
                    1.1
                            0.3
                                 18.1
                                                        4-174 0-590
                                 34.2
0.90 0.570
             1.22
                    1.5
                            0.4
                                        0.0510 10,118
                                                        4,015 0.466
1.00 0.386
             1.02
                    0.4
                            0.1
                                 3.1
                                        0.0395 14,518
                                                        5,761 0.378
1.10 0.285
             1.00
                    0.0
                            0.0
                               -12.0
                                        0.0369 17,110
                                                        6,790 0.312
```